M2 High-Speed Tool Steel: A Technical Overview of Heat Treatment Procedures

Abstract: The optimal performance of M2 high-speed tool steel in demanding applications, such as cutting tools and dies, is critically dependent on precise heat treatment. This document outlines the metallurgical principles and procedural steps involved in the heat treatment of M2 steel, including preheating, austenitizing, quenching, and tempering. Adherence to these guidelines is essential for achieving the desired microstructure, characterized by tempered martensite and a fine dispersion of hard, complex carbides, which imparts the requisite hardness, wear resistance, and high-temperature properties.

1. Introduction

M2 high-speed tool steel is a tungsten-molybdenum high-speed steel widely utilized for its excellent balance of toughness, wear resistance, and red hardness. The efficacy of M2 steel is intrinsically linked to its microstructure, which is predominantly controlled by the heat treatment process. An improperly executed thermal processing cycle can significantly degrade the material's performance, irrespective of the initial steel quality. The primary objective of heat treating M2 steel is to transform its annealed state, typically consisting of ferrite and alloy carbides, into a hardened and tempered martensitic matrix incorporating specific carbides essential for cutting tool functionality.

2. Metallurgical Principles and Heat Treatment Stages

The heat treatment of M2 high-speed tool steel is a multi-stage process designed to achieve a specific microstructure. This microstructure, typically comprising tempered martensite and finely dispersed "secondary hardening" carbides, is responsible for the material's superior mechanical properties. The process is systematically divided into four key stages: preheating, austenitizing, quenching, and tempering.

2.1 Preheating

While not directly contributing to the hardening reaction, preheating is a critical preparatory step with several vital functions:

- **Thermal Shock Mitigation:** Preheating minimizes the risk of thermal shock, distortion, or cracking when cold components are introduced into high-temperature austenitizing furnaces.
- Stress Relief: It aids in relieving residual stresses induced during prior machining

or forming operations.

- **Process Efficiency:** Preheating can reduce the overall time required in the high-heat austenitizing furnace, thereby enhancing productivity.
- **Surface Integrity:** In non-neutral furnace atmospheres, preheating can reduce the extent of surface carburization or decarburization.

For M2 steel, a two-step preheat is often recommended, particularly in salt bath hardening. The initial preheat is typically conducted at 650-760°C (1200-1400°F), followed by a second preheat at 815-900°C (1500-1650°F). In atmosphere or vacuum furnaces, a single preheat in the range of 790-845°C (1450-1550°F) is common. Specific preheat temperatures for M2 frequently include 650°C (1200°F) or 815°C (1500°F). The soaking time at preheat temperature should be sufficient to ensure uniform heating throughout the component's cross-section, typically 10 to 12 minutes for M2. Unlike some other tool steels (e.g., D2), which benefit from slow heating, high-speed steels like M2 respond optimally to a rapid temperature increase from the preheat to the austenitizing temperature.

2.2 Austenitizing (Hardening)

Austenitizing is the critical high-temperature stage where the steel is heated to dissolve complex alloy carbides into the austenite matrix. This dissolution is fundamental to achieving the desired hardened properties.

- **Temperature Range:** High-speed tool steels necessitate austenitizing temperatures very close to their solidus temperature, typically within 28-56°C (50-100°F) of it. The general austenitizing range for these steels is 1150-1290°C (2100-2350°F). For M2 steel, the recommended austenitizing temperature is approximately 1230°C (2250°F).
- Holding Time: The holding time at the austenitizing temperature is relatively short, generally 2 to 6 minutes. This duration is contingent upon the specific M2 grade, tool geometry, and cross-sectional thickness. For instance, a 150 mm (6-inch) thick section may require a maximum hold time of 5 to 6 minutes.
- **Atmosphere Control:** Due to the high temperatures involved, maintaining a controlled furnace atmosphere (e.g., neutral salt bath, vacuum, or controlled atmosphere furnace) is crucial to prevent surface degradation phenomena such as scaling and decarburization.
- **Microstructural Transformation:** During austenitizing, the initial ferritic matrix and alloy carbides transform into an austenitic grain structure. The carbon and alloying element content in the austenite, governed by the austenitizing temperature, dictates the as-quenched hardness and the volume fraction of retained austenite. Higher austenitizing temperatures generally correlate with

higher achievable hardness after secondary hardening.

2.3 Quenching

Following austenitization, rapid cooling (quenching) is performed to transform the austenite into martensite, the desired hard microstructural constituent.

- Quenching Media: M2 high-speed tool steel can be quenched in various media, including oil, air, or a neutral salt bath. Air cooling is the least severe method and is suitable for smaller or thinner sections where a sufficient cooling rate can be achieved to form martensite. Oil quenching is often followed by air cooling to near ambient temperature. Salt bath quenching is typically performed in baths maintained at 540-595°C (1000-1100°F).
- **Quenching Technique:** Proper immersion techniques are vital to minimize distortion and thermal stresses. Components with flat sections should be immersed vertically. Tubular sections should also be quenched in a vertical orientation.
- Cooling to Ambient Temperature: It is imperative to cool the component to at least 65°C (150°F) before tempering.
- Retained Austenite: High-carbon, high-alloy steels like M2 invariably exhibit a significant amount of retained austenite after quenching, as the martensitic transformation (Ms-Mf) is rarely complete. Retained austenite can adversely affect hardness, strength, and dimensional stability. Subzero treatments (cryogenic treatments), typically between -30°C and -120°C, can be implemented after an initial temper to promote the transformation of retained austenite to martensite, thereby enhancing hardness and dimensional stability.

2.4 Tempering

Tempering (drawing) is the final, indispensable stage following quenching. The as-quenched steel is in a highly stressed and brittle condition.

- **Primary Functions:** Tempering serves to increase toughness, relieve internal stresses, and induce "secondary hardening" a characteristic phenomenon in many alloyed tool steels. It is also critical for transforming any retained austenite (which may transform to untempered martensite upon cooling from the first temper) into tempered martensite. Precipitation of fine, complex carbides during tempering contributes significantly to secondary hardness.
- **Multiple Tempering:** Due to the transformation of retained austenite to fresh, untempered (and thus brittle) martensite upon cooling from the first tempering cycle, high-speed tool steels universally require multiple tempering operations. This ensures that all martensite present is adequately tempered. M2 steel typically

requires a minimum of two tempers (double tempering), with three tempers often preferred. Each tempering cycle usually involves a soak time of 2 to 4 hours. This multi-stage tempering refines the microstructure, enhancing wear resistance and tool longevity.

- Tempering Temperatures and Duration: For M2, the minimum tempering temperature is generally 540°C (1000°F). A common and effective tempering regime for M2 involves a first temper at 565°C (1050°F), a second temper at 550°C (1025°F), and potentially a third temper at 540°C (1000°F). Each cycle should last for approximately 2 hours per 25 mm (1 inch) of cross-sectional thickness.
- Inter-Temper Cooling: It is crucial to allow the component to cool to room temperature between tempering cycles. This cooling facilitates the transformation of any remaining retained austenite to martensite, which is then tempered in the subsequent cycle.
- Secondary Hardening Peak: To optimize the transformation of retained austenite and maximize secondary hardness, tempering parameters should be selected to target the high-temperature side of the secondary hardening peak on the tempering response curve. M2 relies on this secondary hardening effect to maintain hardness at elevated operating temperatures encountered during high-speed machining.

3. Resultant Microstructure and Hardness

A correctly executed heat treatment process transforms the initial ferrite and coarse carbides of annealed M2 steel into a microstructure predominantly composed of tempered martensite and a fine, uniform dispersion of hard alloy carbides. This optimized microstructure is directly responsible for achieving the desired balance of hardness, wear resistance, and fracture toughness. General-purpose M2 high-speed tool steels are typically heat-treated to a hardness range of 64-66 HRC. However, through meticulous control of austenitizing and tempering parameters, particularly to optimize carbide dissolution and precipitation, hardness values of 68 HRC, and in some specialized cases (analogous to M42), up to 70 HRC can be attained.

4. Conclusion

The successful deployment of M2 high-speed tool steel is contingent upon a rigorously controlled and meticulously executed heat treatment regimen. Strict adherence to the specified temperature ranges, holding times, and procedural sequences for preheating, austenitizing, quenching, and particularly the multi-stage tempering process, is paramount to unlocking the full performance potential of this

material. This ensures the development of an optimal microstructure, leading to superior hardness, wear resistance, and toughness, which are critical for demanding industrial applications. It is always advisable to consult the specific recommendations provided by the steel manufacturer, as minor variations in chemistry and processing can exist between different heats and suppliers.

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